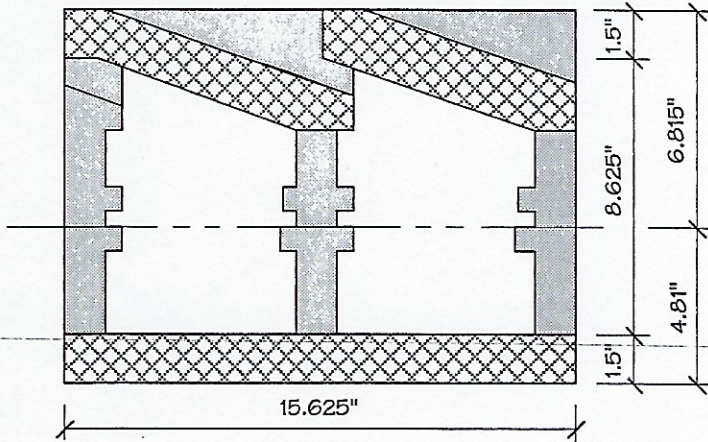


THEORETICAL STRESS ANALYSIS



12" SOUND CELL™

BEDDED AREA CROSS HATCHED

GROSS AREA: $11.625 \times 15.625 = \underline{181.6 \text{ in}^2}$

NET AREA:

$$1.5 \times 15.625 = 23.4375 \quad \times 8.865 = 207.77$$

$$1.5 \times 15.625 = 23.4375 \quad \times 0.75 = \underline{17.58}$$

$$\underline{225.35}$$

BEDDED AREA: $2 \times 1.5 \times 15.625 = \underline{46.875 \text{ in}^2}$

$$+ 2 \times 1.25 \times 6.375 = 15.9375$$

$$+ 1 \times 1.25 \times 7.75 = \underline{9.6875}$$

* NET AREA: $\quad \quad \quad = \underline{72.50 \text{ in}^2}$

$$y = 225.35 \div 46.875 = \underline{4.81 \text{ in}} \quad (6.815)$$

$$I_{\text{NET}} = (2 \times 15.625 \times 1.5^3) \div 12 = 8.79$$

$$+ 1.5 \times 15.625 \times 6.063^2 = 862.13$$

$$+ 1.5 \times 15.625 \times 4.06^2 = \underline{386.33}$$

* $I_{\text{NET}} = 1257.25 \text{ in}^4$

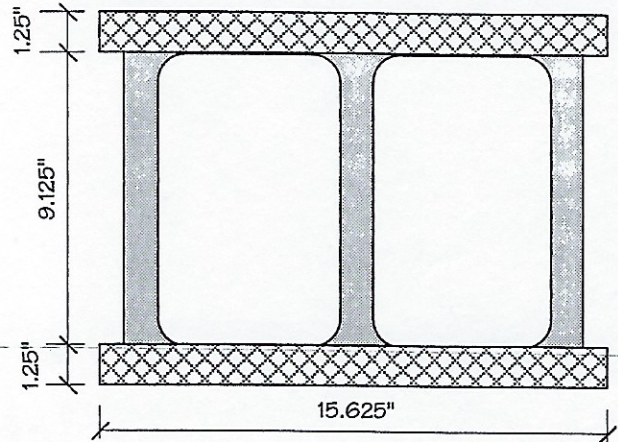
or = $\underline{965.57 \text{ in}^4/\text{ft}}$

$$S_{\text{BEDEXT}} = 1257.25 \div 4.81 = \underline{261.38 \text{ in}^3}$$

$$S_{\text{BEDEXT}} = \underline{200.74 \text{ in}^3/\text{ft}}$$

$$S_{\text{BEDINT}} = 1257.25 \div 6.815 = \underline{184.48 \text{ in}^3}$$

$$S_{\text{BEDINT}} = \underline{141.68 \text{ in}^3/\text{ft}}$$



STANDARD 12" C.M.U.

BEDDED AREA CROSS HATCHED

GROSS AREA: $11.625 \times 15.625 = \underline{181.6 \text{ in}^2}$

NET AREA:

$$2 \times 1.25 \times 15.625 = 39.06 \text{ in}^2$$

$$+ 2 \times 1.50 \times 9.125 = 27.38$$

$$+ 1 \times 1.25 \times 9.125 = 11.41$$

$$+ 12 \times 0.084 = \underline{01.00}$$

* NET AREA: $\quad \quad \quad = \underline{78.85 \text{ in}^2}$

$$I_{\text{NET}} = (2 \times 15.625 \times 1.25^3) \div 12 = 5.086$$

$$+ 2 \times 15.625 \times 1.25 \times 4.625^2 = 835.571$$

* $I_{\text{NET}} = 840.66 \text{ in}^4$

or = $\underline{645.60 \text{ in}^4/\text{ft}}$

$$S_{\text{BEDEXT}} = 840.66 \div 5.8125$$

$$S_{\text{BEDEXT}} = \underline{144.63 \text{ in}^3} \quad \text{or} \quad \underline{111.1 \text{ in}^3/\text{ft}}$$

(OVER)

THEORETICAL STRESS ANALYSIS:

Apply Load "P" & Moment "M" / Lin. Ft.

$$A = 2 \times 1.5 \times 12$$

$$A = \underline{36 \text{ in}^2}$$

$$f_a = 1 = (P \div A_{BED})$$

$$f_a = 1 = (P \div 36)$$

$$f_a = \underline{0.0277 P}$$

$$f_{b_{INT}} = (M \div S_{BED_{EXT}}) = (M \div 200.74)$$

$$f_{b_{INT}} = \underline{0.0041 M}$$

$$f_{b_{EXT}} = (M \div S_{BED_{INT}}) = (M \div 141.68)$$

$$f_{b_{EXT}} = \underline{0.007 M}$$

THEORETICAL STRESS ANALYSIS:

Apply Load "P" & Moment "M" / Lin. Ft.

$$A = 2 \times 1.25 \times 12$$

$$A = \underline{30 \text{ in}^2}$$

$$f_a = 1 = (P \div A_{BED})$$

$$f_a = 1 = (P \div 30)$$

$$f_a = \underline{0.0333 P}$$

$$f_b = (+/- M \div S_{BED}) = (M \div 111.1)$$

$$f_b = +/- \underline{0.009 M}$$

CONCLUSIONS

SINCE AXIAL & FLEXURAL STRESSES f_a & f_b ARE LOWER ON THE SOUND CELL™ UNIT THAN ON THE STANDARD 12" C.M.U., A 12" SOUND CELL™ UNIT CAN BE CONSIDERED THE EQUIVALENT OF A STANDARD 12" C.M.U.